

# Thermal Stability of High Performance Thermoelectric $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> in Argon

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The stability of the high performance thermoelectric  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> is investigated by multi-temperature high resolution synchrotron powder X-ray diffraction. Contrary to previous claims  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> is not stable when heated in argon and degradation is observed already at 500 K. Nevertheless, the thermal stability of  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> is much improved in argon (ca. 5 wt.-% degradation after three heating cycles to 625 K) relative to heating in atmospheric air (ca. 60 wt.-% degradation). Based on identification of the decomposition products

two specific degradation processes are proposed, and the excellent stability of  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> synthesized by zone melting (equilibrium method) is discussed in relation to the poor stability of material synthesized by thermal quenching (non-equilibrium process). The room temperature peak widths and unit cell parameters change significantly after three heating cycles to 625 K suggesting that the  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> phase diagram could be more complex than currently believed.

## Introduction

Increasing pressure on the environment and the energy supply has revived interest in the search for more efficient thermoelectric materials. The  $\beta$ -phase of Zn<sub>4</sub>Sb<sub>3</sub> has been found to be an excellent *p*-type thermoelectric semiconductor when used in the intermediate temperature range (473–673 K).<sup>[1]</sup> The thermoelectric figure of merit is defined as  $zT = S^2\sigma T/\kappa$ , where  $S$  is the thermopower,  $\sigma$  the electrical conductivity,  $\kappa$  the thermal conductivity ( $\kappa_{\text{lattice}} + \kappa_{\text{electronic}}$ ) and  $T$  the absolute temperature. Good thermoelectric materials are typically strongly doped semiconductors with complex structures and large unit cells, which favor the preservation of a high power factor ( $S^2\sigma$ ), while various phonon scattering processes lowers the thermal conductivity.<sup>[2–5]</sup> It is three disordered interstitial Zn sites which endow  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> an unusually low thermal conductivity and makes it a competitive thermoelectric candidate.<sup>[3]</sup>  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> has received considerable interest also because it is among the cheapest thermoelectric materials known, and it is made of non-toxic elements.<sup>[6–8]</sup> However, the real thermoelectric performance of Zn<sub>4</sub>Sb<sub>3</sub> can be difficult to assess because the material decomposes in the expected working temperature range.<sup>[1,5,9]</sup> Thermal stability of a material is a prerequisite for being able to define a proper material  $zT$  value. If a material decomposes during measurement of the properties then clearly the “ $zT$  value” will not relate to the specific material and it will give limited information about the po-

tential thermoelectric performance of the compound. The situation gets even more problematic in practice, because the individual parameters of  $zT$  typically are measured separately and often on different samples. The latter in itself introduces a systematic bias, but if the material is not thermally stable then multiplication of the individually measured values of  $S$ ,  $\sigma$ , and  $\kappa$  has limited use.

$\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> was originally reported to be stable up to 673 K in argon, and up to 523 K in dynamic vacuum.<sup>[1,2]</sup> When held at elevated temperatures, the compound partly decomposed but the specific products and quantitative degree of the decomposition were not reported. The originally reported thermal stability has been questioned by several authors. They found that  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> starts to decompose at temperatures below the expected temperature,<sup>[9]</sup> by losing Zn,<sup>[10]</sup> and forming ZnSb and Zn as decomposition products.<sup>[5]</sup> Iversen and co-workers reported the instability of the material even below 500 K with formation ZnSb, ZnO and elemental Sb as degradation products.<sup>[11]</sup> An onset temperature of 469 K was reported by Erk et al. in the study of metastable nanocrystalline Zn<sub>4</sub>Sb<sub>3</sub>.<sup>[12]</sup> It has been shown that  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> synthesised by thermal quenching decomposes very substantially when heated in atmospheric air,<sup>[11]</sup> whereas material synthesised by zone melting exhibits a remarkable stability.<sup>[11,13]</sup> Since the properties of  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> synthesized by thermal quenching and by zone melting are different, it follows that the crystal structures and/or microstructure of the two materials must be different. The decomposition in air is problematic if the material is to be used in an actual thermoelectric device, but the reported  $zT$  values could still be valid since high temperature properties typically are measured in argon or vacuum. Clearly, it is important for the understanding of  $\beta$ -Zn<sub>4</sub>Sb<sub>3</sub> that the thermal stability of the structure is established during heating

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in argon. It should also be mentioned that doping of  $\text{Zn}_4\text{Sb}_3$  has been shown by Iversen et al. as a way to improve the stability.<sup>[14,15]</sup> In the present work, we study the degradation behavior of quench synthesised  $\beta\text{-Zn}_4\text{Sb}_3$  by heating the sample in argon atmosphere while measuring high resolution synchrotron powder X-ray diffraction (PXRD) data.

## Results and Discussion

Selected crystallographic parameters are listed in Table 1 for the data recorded at 300 K before and after heating. Even with a third-generation synchrotron source, which routinely makes crystalline phases down to a 0.1 wt.-% level detectable,<sup>[16]</sup> no impurities were observed in both samples before heating. The refined stoichiometries of the two samples are  $\text{Zn}_{38.6}\text{Sb}_3$  and  $\text{Zn}_{38.3}\text{Sb}_3$  for Air and Ar sample, respectively.

Table 1. Crystallographic details and refinement residuals for the sample heated in argon (Ar) and in air (Air). "start" refers to refinement of the data set recorded before heating, and "after" refers to refinement of the data set recorded at 300 K after three heating cycles.

	Ar, start	Air, start	Ar, after	Air, after
$T/\text{K}$	300	300	300	300
$t_{\text{exp}}/\text{min}$	5	5	5	5
Points	7861	7507	7867	7507
Reflections	5217	4863	5164	4682
Parameters	78	90	97	116
$R_F/\%$	1.58	1.34	2.64	2.83
$R_{\text{Bragg}}/\%$	1.84	1.84	2.65	2.71
$R_p/\%$	2.85	2.39	3.62	4.06
$R_{\text{wp}}/\%$	3.94	3.15	4.79	6.16
$\chi^2$	6.63	2.91	8.09	12.50
$a = b/\text{\AA}$	12.2183(2)	12.2257(1)	12.2329(2)	12.2383(2)
$c/\text{\AA}$	12.4044(2)	12.4162(1)	12.4249(2)	12.4256(2)
$X$	0.193(4)	0.241(4)	0.122(3)	0.218(4)
$Y$	0.013(0)	0.023(4)	0.005(0)	0.0001(0)
$B_{\text{iso}} \text{ Sb1}$	1.13(3)	1.26(2)	0.98(3)	1.01(5)
$B_{\text{iso}} \text{ Sb2}$	1.00(3)	1.25(3)	0.92(3)	0.94(6)
$B_{\text{iso}} \text{ Zn}$	2.04(6)	2.11(5)	2.10(5)	2.11(11)
Occ Sb1	1	1	1	1
Occ Sb2	1	1	1	1
Occ Zn1	0.941(4)	0.905(3)	0.951(3)	0.944(7)
Occ Zn2	0.049(2)	0.052(1)	0.057(2)	0.065(4)
Occ Zn3	0.031(2)	0.047(2)	0.028(2)	0.034(5)
Occ Zn4	0.038(2)	0.032(1)	0.046(2)	0.045(4)
$V/\text{\AA}^3$	1603.7(0)	1607.2(3)	1610.2(0)	1611.7(4)
Wt.-% ZnSb	0	0	2.9(1)	4.0(2)
Wt.-% ZnO	0	0	0	21.1(4)
Wt.-% Sb	0	0	2.6(0)	32.3(2)

Further details of the multi-temperature refinement are provided in Supporting Information for both samples.

The synchrotron powder diffraction patterns of the two samples, before and after heating to 625 K in the different atmospheres are shown in Figure 1. The difference in thermal behaviors is notable. A large number of additional peaks appear in the sample heated in air, and these are identified by the Rietveld refinement to be the decomposition products: ZnSb, ZnO and elemental Sb (details are shown in Table 1). In contrast, the patterns from the sample heated

in argon are similar and only a couple of additional impurities peaks appear after heating. This directly shows that the degradation is much more limited for the sample heated in an inert atmosphere. Figure 2(a) plots the weight fraction of the starting phases as determined by Rietveld refinement during the first heating (300  $\rightarrow$  625 K) of the two samples. It is clearly seen that both samples start to decompose before 500 K, and in the sample heated in air almost 4% of original phase has been lost at 500 K. Further heating accelerates the degradation, and only 65 wt.-%  $\text{Zn}_4\text{Sb}_3$  is left at 625 K generating about 20 wt.-% Sb, ca. 10 wt.-% ZnO and ca. 5 wt.-% ZnSb as decomposition products, see Figure 2 (b).

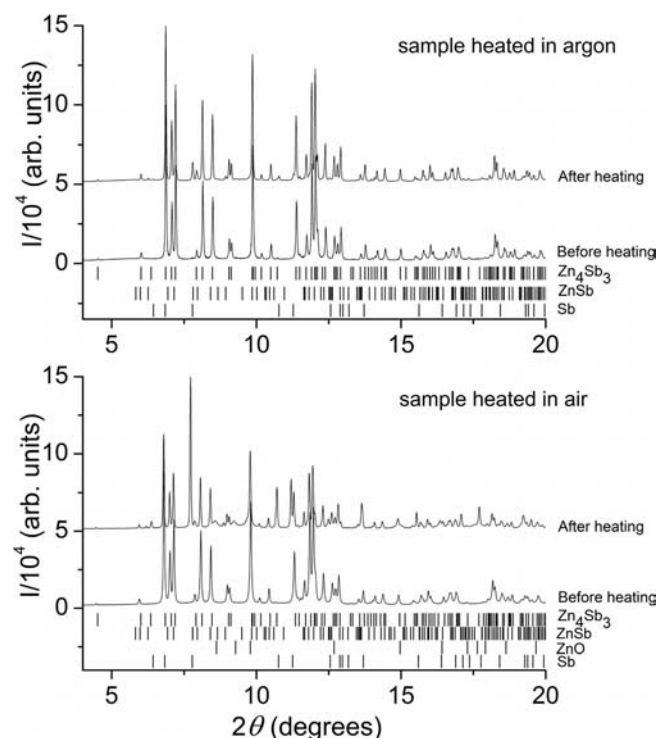


Figure 1. Powder patterns of  $\text{Zn}_4\text{Sb}_3$  heated in argon (above) and heated in air (below) recorded at 300 K before heating, and after three heating cycles. The vertical lines correspond to the position of Bragg peaks of corresponding phases.

The decomposition behavior of the sample heated in argon is very different, see Figure 2 (a). A slight weight loss occurs below 500 K, followed by continuous but limited decomposition, of which the rate seems to decrease. At 625 K more than 96 wt.-% of the starting  $\text{Zn}_4\text{Sb}_3$  material remains. Iversen et al.<sup>[11]</sup> studied a zone-melted  $\text{Zn}_4\text{Sb}_3$  sample, which was found to be stable within 300 K to 625 K except for an isolated event at ca. 523 K, where a subtle decomposition is observed. Here, we observe a continuous degradation during the temperature range under study, corroborating that the thermal behavior of  $\text{Zn}_4\text{Sb}_3$  is affected by synthesis methods. As expected, no oxidation impurities appear during the decomposition in argon, and the decomposition products are ZnSb and elemental Sb, see Figure 2 (b). However, these two products are incompatible with the stoichiometry. Additional elemental Zn, or other Zn com-

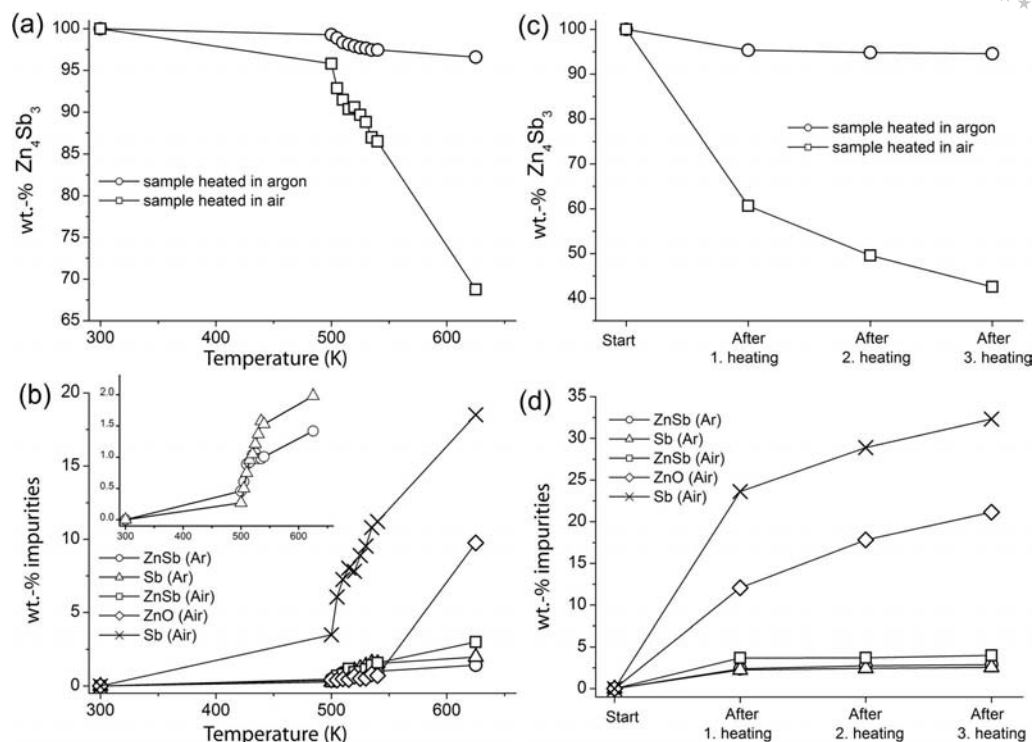


Figure 2. a) Weight fraction of remaining  $\text{Zn}_4\text{Sb}_3$  as a function of temperature in the first heating cycle. b) Weight fraction of impurity phases  $\text{ZnSb}$ , ( $\text{ZnO}$ ) and  $\text{Sb}$  as a function of temperature in the first heating cycle. c) Weight fraction of remaining  $\text{Zn}_4\text{Sb}_3$  as a function of heating cycles. d) Weight fraction of impurity phases  $\text{ZnSb}$ , ( $\text{ZnO}$ ) and  $\text{Sb}$ , as a function of heating cycles.

pounds, must form when the 4:3 phase degrades into the 1:1 phase and elemental  $\text{Sb}$ . As the capillaries were sealed, no substances can escape and it appears that the missing  $\text{Zn}$  must be present either in an undetected amorphous phase or disappear due to sublimation.

Part c of Figure 2 shows the weight fraction of the remaining  $\text{Zn}_4\text{Sb}_3$  phase in both samples determined at 300 K after each of the three heating cycles. The sample heated in air seems to continue degrading during the first cooling down to 300 K and an additional ca. 5 wt.-% of the original phase is lost. Additional heating causes further decomposition leaving only ca. 40 wt.-%  $\text{Zn}_4\text{Sb}_3$  after three cycles. The sample heated in argon is much more stable than that heated in air and the decomposition rate indeed is small. More than 94 wt.-% of the starting phase is still remaining after three heating cycles, and it appears that during further heating cycles  $\text{Zn}_4\text{Sb}_3$  will reach a “plateau” of decomposition. The refined weight fractions of decomposition impurities for both samples are shown in Figure 2 (d). For a sample synthesized by zone melting the corresponding weight percentages were 4.8%  $\text{ZnSb}$ , 2.5%  $\text{ZnO}$  and 1.6%  $\text{Sb}$ ,<sup>[11]</sup> while for a 1% Cd-doped sample synthesized by the quench method the weight percentages were 4.5%  $\text{ZnSb}$ , 8.4%  $\text{ZnO}$  and 8.8%  $\text{Sb}$ . (Both samples had the same thermal cycling in atmospheric air as in the present study.<sup>[15]</sup>) For the three pure  $\text{Zn}_4\text{Sb}_3$  samples the amounts of  $\text{ZnSb}$  are similar, whereas the amounts of  $\text{ZnO}$  and  $\text{Sb}$  are distinctly different.  $\text{ZnSb}$  is stable up to at least 800 K according to the phase diagrams.<sup>[17,18]</sup> This implies that the decomposition of  $\text{Zn}_4\text{Sb}_3$  actually consists of two different processes i.

$\text{Zn}_4\text{Sb}_3 \rightarrow \text{ZnSb} + \text{Zn}$ , and ii.  $\text{Zn}_4\text{Sb}_3 \rightarrow \text{Zn} + \text{Sb}$ . The first process (giving rise to  $\text{ZnSb}$ ) occurs to approximately the same extent for all four samples independent of the atmosphere, synthesis method or doping, and this degradation therefore appears to be “intrinsic” to the structure. In molar terms 3.2% of the initial  $\text{Zn}_4\text{Sb}_3$  degrades to  $\text{ZnSb}$  for the quench sample in argon, 4.4% of the quench sample in air, 5.3% of the zone-melted sample in air, and 5.0% of the Cd-doped quench sample heated in air. The extent of the second reaction (monitored by the  $\text{Sb}$  content) is very different in the four cases. For the pure sample heated in argon an additional 4.4 mol.-%  $\text{Zn}_4\text{Sb}_3$  degrades (into  $\text{Zn}$  and  $\text{Sb}$ ), whereas 55.4% degrades during heating of the pure quench samples in air. Thus, when  $\text{Zn}$  is removed from the matrix by reaction with oxygen a very strong decomposition takes place. The corresponding number for reaction 2 for the zone melted sample heated in air is 2.8%, and it is 15.2% for the Cd-doped quench sample heated in air. The major improvement of the zone melted pure sample relative to the quench sample is the suppression of reaction 2 even in an oxygen rich atmosphere, and it only occurs to the same extent as for the sample heated in argon (3–4%). This suggests that the generated  $\text{Zn}$  atoms are not able to escape to the surface of the crystallites and get exposed to oxygen. This may be due to the fewer defects in the zone-melted sample since zone-melting is an equilibrium process, during which crystals gain more perfect lattices. A tracer diffusion study shows that  $\text{Zn}$  is highly mobile in the structure.<sup>[19]</sup> Defects should make it easier for  $\text{Zn}$  atoms to diffuse. The extent of reaction 2 is also greatly suppressed for Cd-doped sam-

ples with a decrease in  $\text{Zn}_4\text{Sb}_3$  decomposition from 55.4% to 15.2%. This is believed to be attributed to the bigger and heavier Cd atoms acting as stabilizers to the structure blocking against Zn diffusion in the lattice. The analysis shows that generation of Zn is common to both reactions, and thus one would predict that addition of Zn to the  $\text{Zn}_4\text{Sb}_3$  matrix should reduce the decomposition and this has indeed been observed.<sup>[13]</sup>

The room temperature unit cell parameters and the peak width (FWHM) of the (300) reflection indexed in the  $\beta\text{-Zn}_4\text{Sb}_3$  phase for samples heated in argon and in air after each heating cycles are plotted in Figure 3.

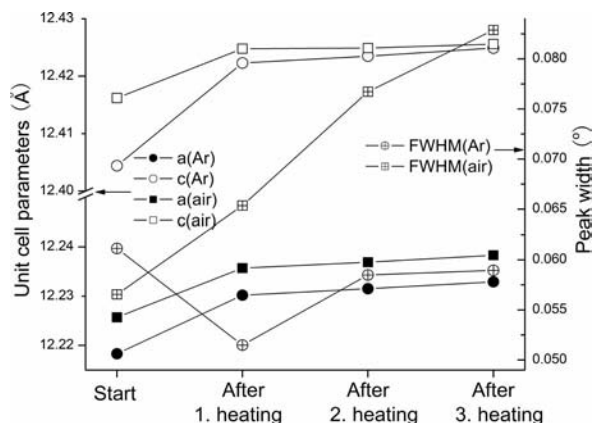


Figure 3. The changes of unit cell parameters (left axis) and peak width (FWHM) of reflection (300) indexed in  $\text{Zn}_4\text{Sb}_3$  (right axis) against heating cycles. The estimated standard uncertainty of each unit cell parameter is below 0.0002 Å.

Since the peak profile was described by a combination of Gaussian and Lorentzian functions, the FWHM were calculated by<sup>[20]</sup>

$$FWHM^5 = H_G^5 + 2.69269H_G^4H_L + 2.42843H_G^3H_L^2 + 4.47163H_G^2H_L^3 + 0.07842H_GH_L^4 + H_L^5$$

where  $H_G$  and  $H_L$  are the individual Gaussian and Lorentzian FWHM components. They are given by the expressions

$$H_G^2 = U \cdot \tan^2 \theta + V \cdot \tan \theta + W$$

$$H_L = X \cdot \tan \theta + Y / \cos \theta$$

and the parameters  $U$ ,  $V$ ,  $W$ ,  $X$ ,  $Y$  are obtained from the Rietveld refinement. Before heating, the values of the unit cell parameters are  $a = 12.2183(2)$  Å,  $c = 12.4044(2)$  Å and  $a = 12.2257(2)$  Å,  $c = 12.4162(2)$  Å for the argon and the air samples, respectively. These values are comparable to our previous studies and to the values reported by Snyder et al., which were based on similar data as the present.<sup>[3,11]</sup> However, they are lower than those reported by other authors based on different types of data.<sup>[21,22,23]</sup> When the samples are heated to 625 K and then cooled to room temperature, the unit cell parameters increase monotonously. After three heating cycles to 625 K, the increase in the room temperature unit cell parameters levels off. In principle, the unit cell parameters of the two samples should be identical

before the start of the experiments, since the samples were from the same synthesis batch and underwent similar preparation. Despite of the systematic error between the two data sets, it appears that the relative change for both samples is clear (ca. 0.01 Å compared with an estimated standard uncertainty of ca. 0.0002 Å), and that the unit cell parameters increase with thermal cycling.

The behaviour of the peak width is quite different for the samples heated in air and in argon. For the sample heated in air there is a significant increase in peak width, which appears to continue with further heating cycles. On the other hand, for the sample heated in argon the behaviour is tricky. The peak width first decreases after one heating cycle, and during the two subsequent cycles increases back to near the starting value. The changes in unit cell parameters and peak widths of  $\beta\text{-Zn}_4\text{Sb}_3$  indicate that not only does the material decompose, but the crystal structure and/or microstructure of the phase itself changes. The peak broadening and unit cell changes could in reality mask that distinct new phases with very similar unit cell parameters are formed from the parent phase. Further investigations are needed to clarify if this is the case.

## Conclusions

In summary, it is found that  $\beta\text{-Zn}_4\text{Sb}_3$  is not as previously reported stable during heating in argon. Based on identification of the decomposition products from different  $\beta\text{-Zn}_4\text{Sb}_3$  samples heated in air and in argon it is proposed that the degradation of  $\text{Zn}_4\text{Sb}_3$  consists of two processes: i.  $\text{Zn}_4\text{Sb}_3 \rightarrow 3 \text{ZnSb} + \text{Zn}$ , and ii.  $\text{Zn}_4\text{Sb}_3 \rightarrow 4 \text{Zn} + 3 \text{Sb}$ . Reaction 1 relates to the thermodynamic stability of  $\text{Zn}_4\text{Sb}_3$ , while the oxidation of Zn accelerates reaction 2, and in the case of samples synthesized by thermal quenching the decomposition is more than 55% for samples heated in air. In terms of practical use, it has empirically been observed that the decomposition is suppressed if pellets synthesized by the quench method are hot-pressed with additional Zn. The two proposed decomposition reactions give a clear explanation for this fact. Due to the severe decomposition material synthesized by thermal quenching must be isolated from oxygen e.g. by coating the legs of the device or protecting the entire module. Material synthesized by zone melting has a strong suppression of reaction 2, which means that it does not suffer from the presence of oxygen. However, such material still benefits from additional Zn during pressing to suppress reaction 1. Since  $\beta\text{-Zn}_4\text{Sb}_3$  is shown not to be stable even at temperatures much below the  $\beta\text{-}\gamma$  phase boundary, reports of  $zT$  values of  $\beta\text{-Zn}_4\text{Sb}_3$  must be interpreted with care. A material  $zT$  value is only really meaningful for materials which are stable, i.e. materials which preserve their identity during the measurement of their properties.

## Experimental Section

**Synthesis and Sample Preparation:** Approximately 70 g of  $\text{Zn}_4\text{Sb}_3$  was prepared by mixing stoichiometric amounts of 99.99% Zn



shots and 99.5% Sb powder in a quartz ampule. The vacuum sealed ampule was placed horizontally into a tube furnace and heated to 973 K with a 400 K/h ramp under continuous rotation for 2 h before quenching in ice water. The resulting polycrystalline, rod shaped sample was ground in an agate mortar and sieved to obtain a grain size less than 45  $\mu\text{m}$ . Homogenous grain size powder, which is important for synchrotron powder diffraction measurement, was obtained by a floating technique. The powders were floated with ethyl alcohol in a Petri dish and left for sedimentation. After 1 min, the top layer of the ethanol was transferred into a new Petri dish, and left for another 1 min for further sedimentation. The top layer was then again moved to a third Petri dish and the ethanol was evaporated, leaving a sample fraction of homogeneous grain size. The samples were filled into 0.2 mm capillaries, followed by about 5 min ultra-sound bath to obtain a dense packing. One capillary was sealed under open air while the other was sealed with epoxy in an argon filled glove box.

**Multitemperature Synchrotron PXRD Recording:** Multi-temperature, high resolution synchrotron PXRD data were recorded using the large Debye-Scherrer camera at beam line BL02B2, SPring8, Japan.<sup>[24]</sup> The data were measured at  $\lambda = 0.42236(1)$  and  $0.42282(0)$  Å for samples heated in air and in argon, respectively, using exposure times of 5 min. The wavelengths were determined from refinements on a  $\text{CeO}_2$  standard. Data were collected at 300 K, between 500–540 K with a step width of 5 K, and at 625 K. After the first heating, the samples were cooled down to 300 K and heated again for another two cycles (i.e. the thermal history was  $300 \rightarrow 625 \rightarrow 300 \rightarrow 625 \rightarrow 300 \rightarrow 625 \rightarrow 300$  K) to imitate a practical application. All data sets were Rietveld refined against the crystal structure model of Snyder et al.<sup>[3]</sup> with the program FULLPROF.<sup>[25]</sup> Data outside the Bragg angle range  $3^\circ < 2\theta < 40^\circ$  were excluded because of low signal-background ratio. A Pseudo-Voigt function with three Gaussian, two Lorentzian, and two asymmetry parameters was found to give a good description of the peak profile, while the background was fitted by linear interpolation among approximately 60 points.

**Supporting Information** (see footnote on the first page of this article): Selected crystallographic details and unit cell parameters for  $\text{Zn}_4\text{Sb}_3$  heated in argon, derived from Rietveld refinement are shown in Table ST1, ST2. Selected crystallographic details and unit cell parameters for  $\text{Zn}_4\text{Sb}_3$  heated in air, derived from Rietveld refinement are shown in Table ST3, ST4.

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